

Chiral Ribbons Formed by Nematic Elastomer Films

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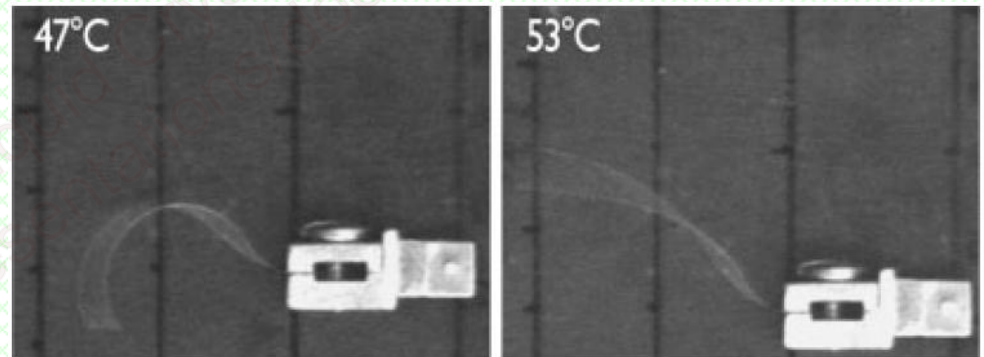
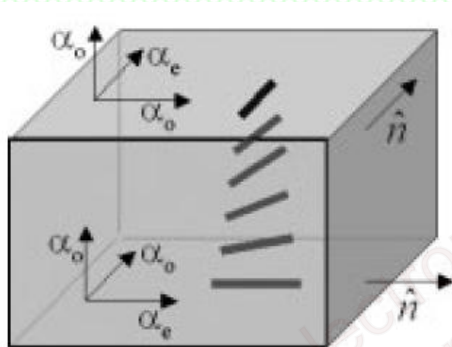
*Liquid Crystal Institute
Kent State University*

Introduction



combination of elasticity
and orientational order

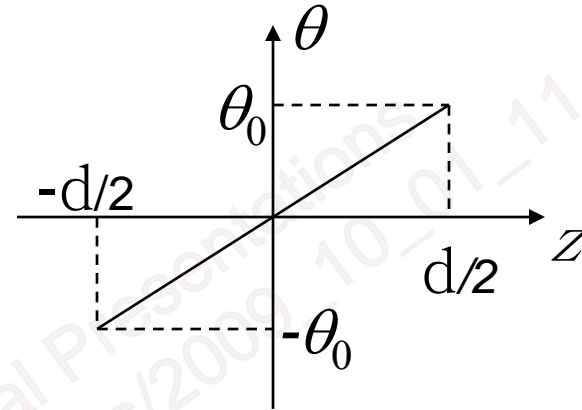
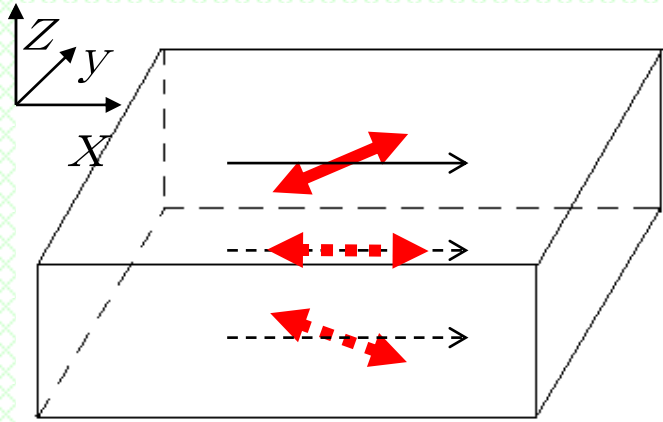
external stimuli \rightarrow shape change



G. Mol *et al*, *Adv. Funct. Mater.*, 2005, **15**, 1155-1159

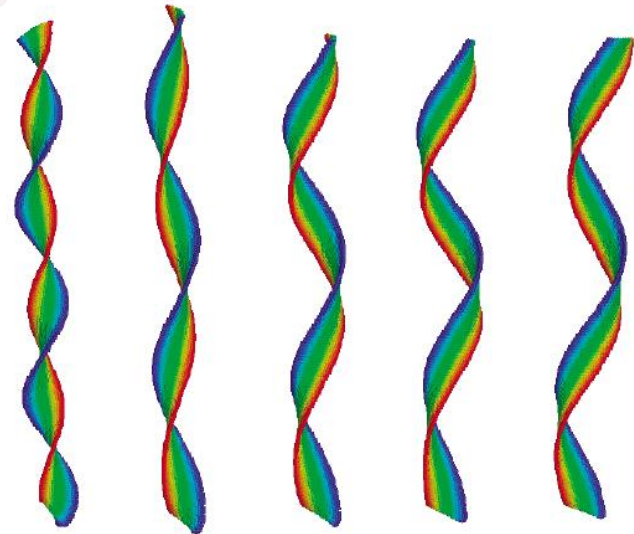
Our goal: to *theoretically* investigate shape change

Theoretic Problem



heating

- nematic to isotropic transition
- expansion/contraction along different axes
- various chiral ribbons



Elastomer Ribbons

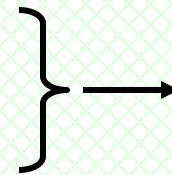
non-isometric



Fopple and von
Karman problem

in-plane elastic energy

out-of-plane bending energy



shape

L.D. Landau and E.M. Lifshitz, *Theory of Elasticity*

Chiral Ribbons

Helicoids



nonzero Gaussian curvature, **zero** bending.

large in-plane stretch energy cost, **no** bending energy cost.

Preferred for **narrow** but **thick** ribbons .

Spiral Ribbons



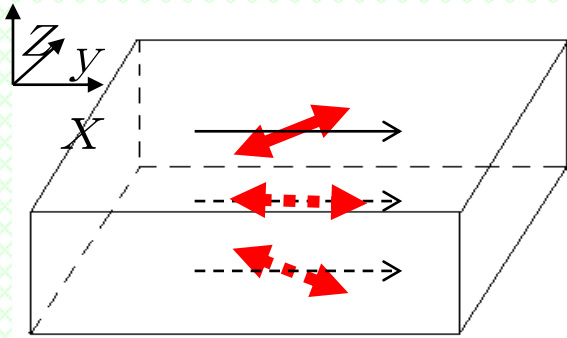
~zero Gaussian curvature, **nonzero** bending.

~no in-plane stretch energy cost, **large** bending energy cost.

Preferred for **wide** but **thin** ribbons .

Elastic Energy

$$f = \mu [\text{Tr } \underline{\underline{\varepsilon}}^2 - \alpha \text{Tr } \underline{\underline{\varepsilon}}(\underline{\underline{Q}} - \underline{\underline{Q}}_0)]$$



$\underline{\underline{Q}}_0$, initial order tensor;

$\underline{\underline{Q}}$, order tensor in body frame vanishes in the isotropic phase.

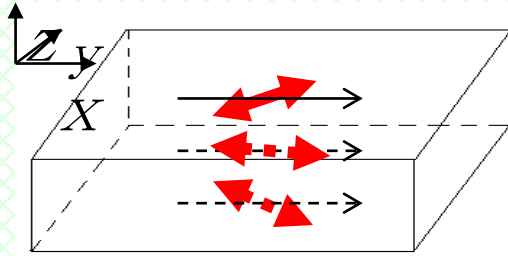
nonlinear strain tensor

$$\varepsilon_{ij} = \frac{1}{2} (\partial_i u_j + \partial_j u_i + \partial_i u_k \partial_j u_k)$$

incompressibility $\rightarrow \varepsilon_{XX} + \varepsilon_{YY} + \varepsilon_{ZZ} = 0$

thin film approximation $\rightarrow \varepsilon_{XZ} = \varepsilon_{YZ} = 0$

2D Effective Energy



Integrating along Z-direction

chiral symmetry breaking term

$$f_{2d} = a_K K^2 + bC_{xy} + a_{xy} (2C_{xy}^2 + K) + a_{xx} C_{xx}^2 + a_{yy} C_{yy}^2$$

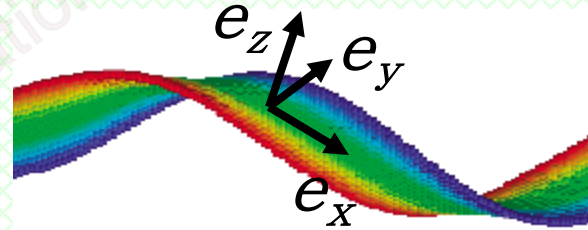
in-plane elastic energy

out-of-plane bending energy

curvature tensor

$$C_{ij} = \partial^2 h / \partial x_i \partial x_j$$

$$K = C_{xx} C_{yy} - C_{xy}^2$$



$$a_{xy} > 0 \implies K < 0$$

Result

$$f = \mu [\text{Tr } \underline{\epsilon}^2 - \alpha \text{Tr } \underline{\epsilon}(\underline{Q} - \underline{Q}_0)]$$

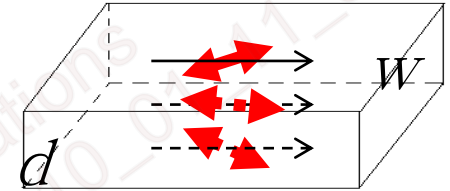
three parameters: w/d , aS , θ_0

$$v = \frac{w}{d} aS \frac{L_{0y}}{L_{0x}^3} \frac{3(\sin 2q_0 - 2q_0 \cos 2q_0)}{(2q_0)^2}$$

$$r = (L_{0x} / L_{0y})^2$$

$$g = \left(\frac{d}{w}\right)^2 \frac{320}{9L_{0x}^2}$$

$$L_{0x} = \left(1 + \frac{1}{2} aS \left(\frac{1}{3} + \frac{\sin 2q_0}{2q_0}\right)\right)^{1/2}, \quad L_{0y} = \left(1 + \frac{1}{2} aS \left(\frac{1}{3} - \frac{\sin 2q_0}{2q_0}\right)\right)^{1/2}$$



For $v < \sqrt{96g / r}$, or $w / d < g(aS, q_0)$

→ Helicoids

$$C_{xx} = 0$$

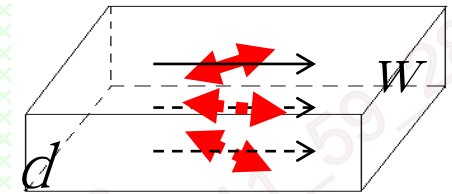
$$C_3 = wC_{xy} : \quad v + 2C_3 / r + 4C_3^3 / (r^2 g) = 0$$



Result

For $v > \sqrt{96g / r}$, or $w / d > g(aS, q_0)$

→ Spiral Ribbons



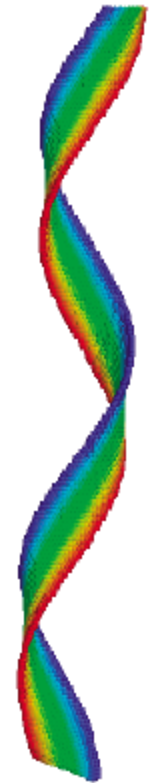
$$C_{xx} w = \sqrt{v^2 r / 64 - 3g / 2}$$

$$C_{xy} w = vr / 8$$

If $w/d \rightarrow \infty$, $C_{xy} \rightarrow \sqrt{r} C_{xx}$, $K \rightarrow 0$

C_{xx} curvature of central line

C_{xy} torsion of central line



Acknowledgement

- NSF Grant DMR-0605889;
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Simulation: Talk TM9

Poster of Gimenez-Pinto

http://www.electronic-crystal.com/docs/2009_11_18_28